

Excercise

OLGA

THE PRACTICAL USE OF "ARCHIE", CONVERSIONS AND ACCURACY.

Introduction:

This example shows logging results used for the determination of hydro-carbon presence and quantities in a reservoir. This method is also used for the definition of:

- coal seam-thickness and the amount of sterile zones in and between coal layers.
- clay type and its purity (for ceramic industrial purposes).
- ore exploration and exploitation (interpretation of the shape of an ore body).
- etc.

In the near future, many Russian oil provinces promise to be the main supplier of hydro-carbons for Western-Europe. Many of these giant oil fields are producing, but are very poorly developed. As a try out, a Dutch/American consortium consisting of oil companies, banks and insurance companies, intend to put a high risk investments in the UTOPIA-field. Many well data have been evaluated. These pre-perestroika figures are produced in a Marxist-Leninist climate and difficult to interpret for "profit-based" exploitation purposes. For this reason a new appraisal well is drilled by DEDRI (Delft Drilling BV i.o.) and evaluated by DUPE (Dutch-Petrophysics V.O.F.). Relevant data, known after drilling, logging and core-evaluation of this well **OLGA - XIII** are:

Well OLGA - XIII

Core and plug results:

- The section 7050 - 7120 ft. was continuously cored.
- The reservoir is a friable sandstone, non-calcareous and shale free.
- The results of the routine core analysis are shown on the log.
- Sidewall samples were taken in the zone 7000 - 7020 ft. This is a hard clean sandstone.
- No oil or gas shows were observed in the samples nor in the mud while drilling through this section.
- Maximum depth logged; 7140 ft.

Drilling information:

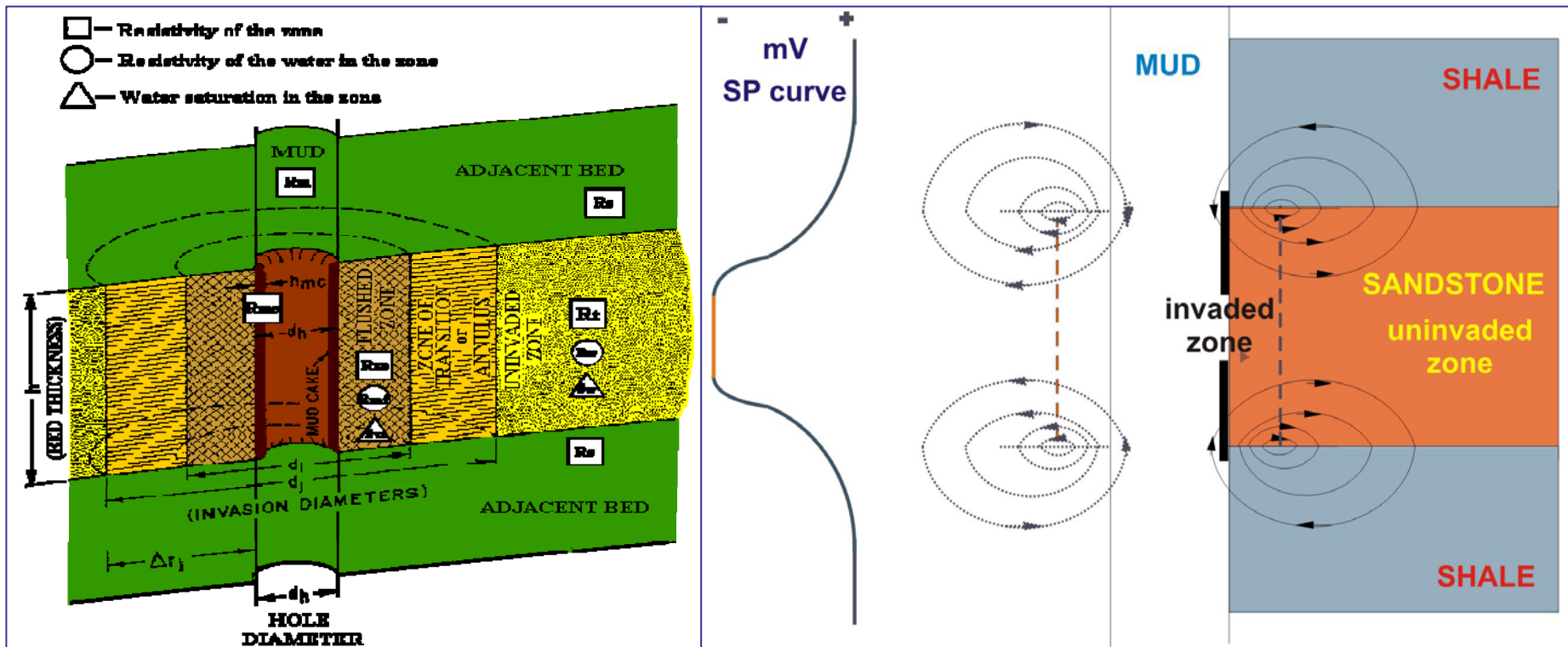
- Bottom hole temperature; 174°F.
- Bit size; 8".
- Mud type; Caustic Quelracho, mud density-10.2 lbs/gal.

Additional information:

- Saturation exponent; $n = 1.6$
- 1 acreft = 1233 m³
- No borehole or bed thickness corrections are required

Define the following in-situ resistivities:

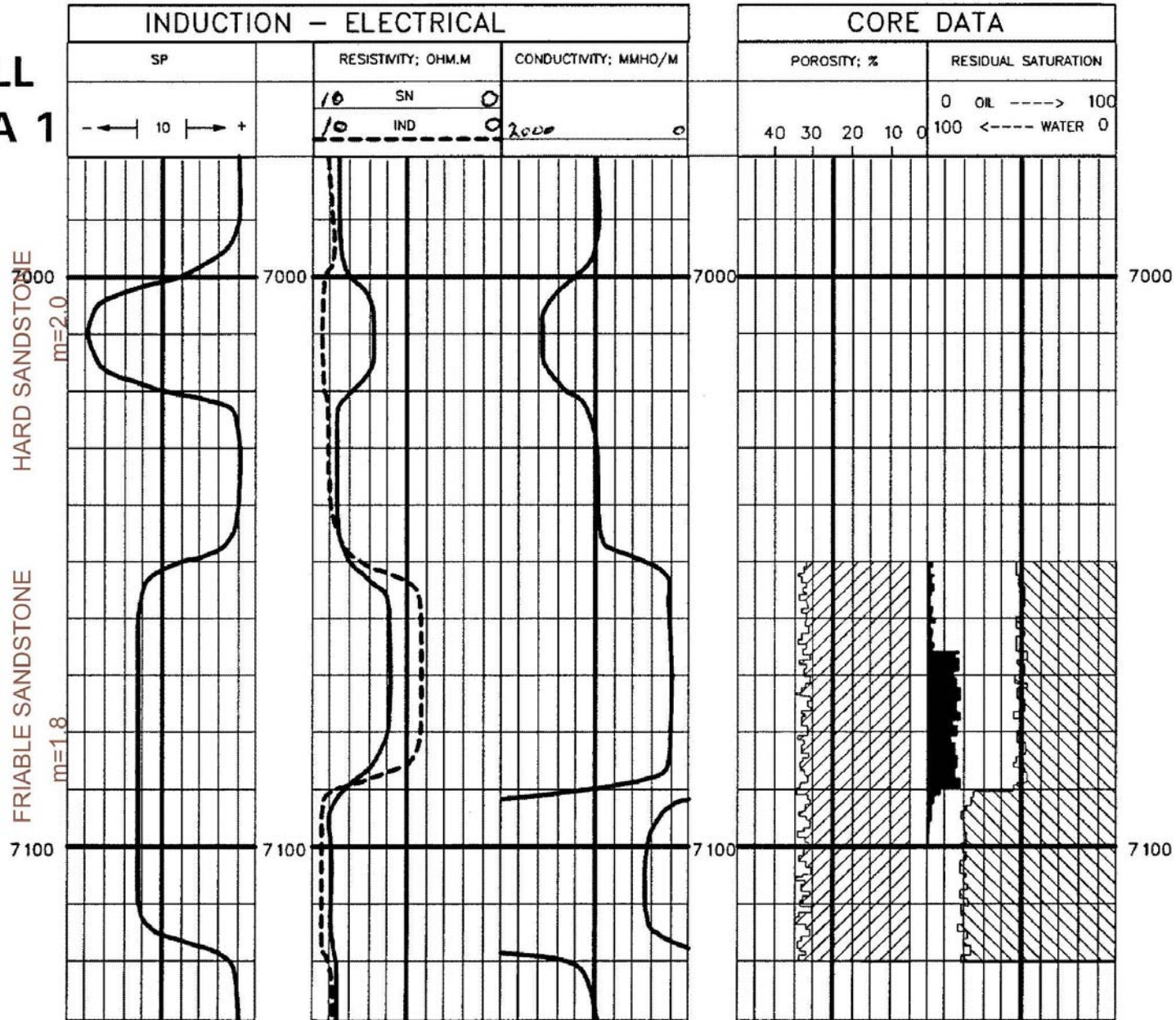
Resistivity mud	0.7 ohm m at 77°F		ohm m at 174°F
Filtrate resistivity	0.5 ohm m at 77°F,		ohm m at 174°F
R _w in the bottom sand	0.14 ohm m at 77°F		ohm m at 174°F
R _w in top sand	0.058 ohm at 77°F		ohm m at 174°F



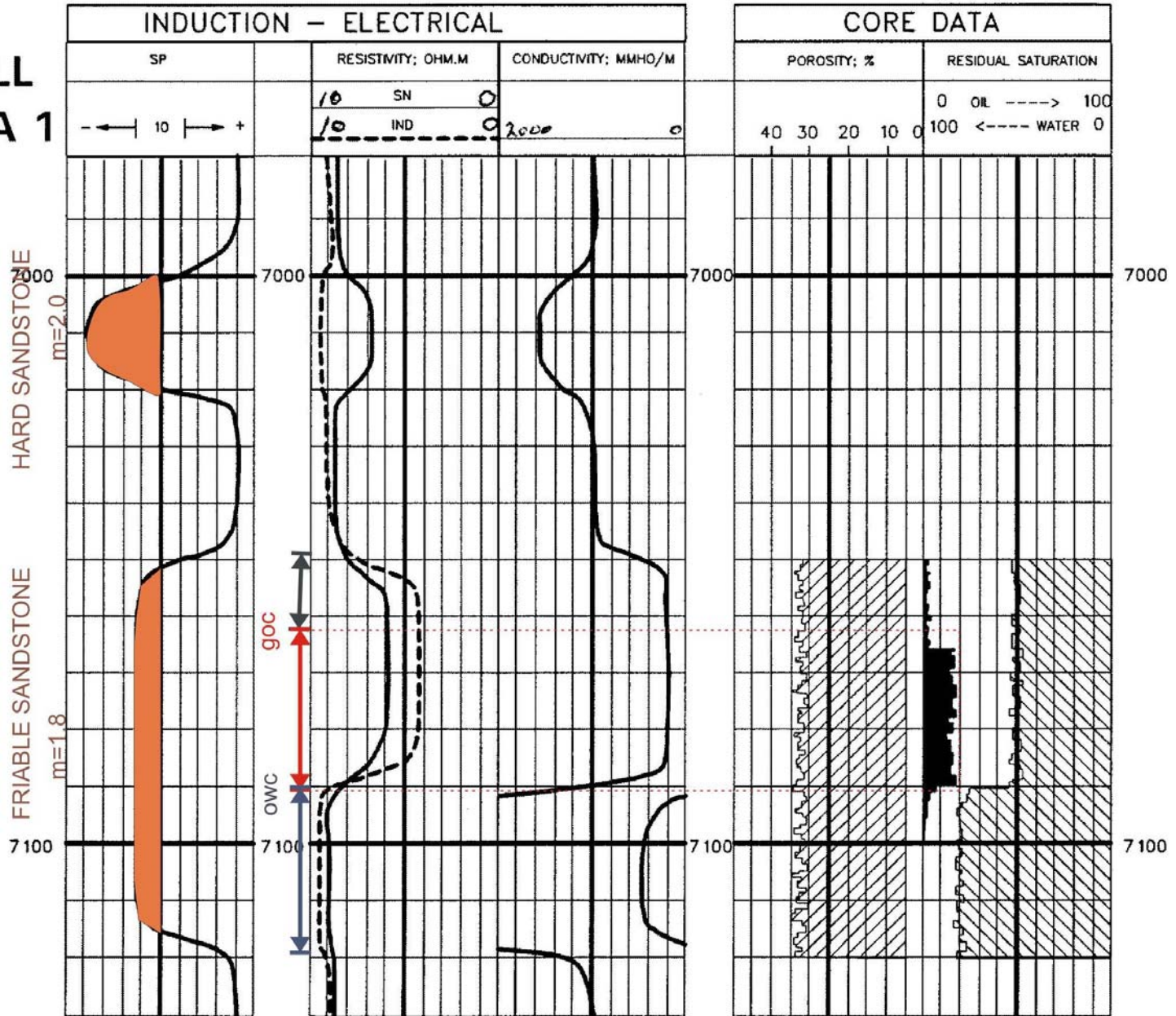
Questions

- 1) What "m" would you consider for the bottom sand?
- 2) What "m" would you consider for the top sand?
- 3) Calculate the amount of Oil In Place in barrels per acre in the lower sandstone,
taking into account the information provided by the core data. (Determine R_o bottom sand in two ways).
- 4) What is the water saturation S_w at 7010 ft.?
- 5) Estimate the porosity of the upper sandstone using;
 - a) the resistivity indicated by the induction log?
 - b) the resistivity indicated by the short normal?
- 6) Are the values found in 5a) and 5b) minimum or maximum values?

WELL OLGA 1



WELL OLGA 1



Define the following in-situ resistivities:

Resistivity mud	0.7 ohm m at 77°F	0.3	ohm m at 174°F
Filtrate resistivity	0.5 ohm m at 77°F,	0.22	ohm m at 174°F
Rw in the bottom sand	0.14 ohm m at 77°F	0.06	ohm m at 174°F
Rw in top sand	0.058 ohm at 77°F	0.024	ohm m at 174°F

OLGA

1. Bottom sand: 7,050-7120 ft $m=1.8$
2. Top sand: 7,000-7020 ft $m=2.0$
3. OIP 7,050-7,120 ft

1 acre = 4046 m², 1 acreft=1233 m³, 1 bbl = 0.1589 m³

Total vol. of 1 acreft = 7758 bbl

OIP = 7758 . h . Porosity . (1 - Sw)

Gross thickness: 70 ft

Gas bearing zone: 7,050-7065 = 15 ft

Below 7065 residual oil in cores

Oil bearing zone: 7,065-7,090 = 25 ft

h = 25 ft

Porosity: atm. = 32 % Cores

in-situ = 28 % ?

porosity = 0.28

Oil saturation:

$$C_t = \text{Por}^{+m} \cdot S_w^{+n} \cdot C_w$$

Ct = 1000/5.7 = 175 (neglecting inv.)

m=1.8, n=1.6, C_w = 15385 mmho/m

$$S_w = 0.255$$

Using in-situ conditions:

$$\text{OIP} = 7758 \times 25 \times 0.28 \times 0.745 = 40,186 \text{ bbl/acre}$$

Using surface conditions:

$$\text{OIP} = 7758 \times 25 \times 0.32 \times 0.78 = 40,186 \text{ bbl/acre}$$

4) What is the water saturation S_w at 7010 ft.?

Answer: $S_w = 1$. Induction high conductivity, lack of shows in SWS (saturated water system)

- 5) Estimate the porosity of the upper sandstone using;
- a) the resistivity indicated by the induction log?
 - b) the resistivity indicated by the short normal?

Answer 5A: induction log: Deep in the formation R_t and S_w can be used.

$$\frac{\text{Formation Water}}{\text{Induction log}} \dots \text{or} \dots \frac{R_o}{R_w} \dots \text{or} \dots \frac{C_w}{C_o} = \phi^{-m}$$

Or:

$$\log \phi = \frac{\log(C_w / C_o)}{-m} \dots \text{valued} \dots \log \frac{(35714 / 1667)}{-2}$$

Then..... $\phi = 0.22$

Answer 5 B: in the invaded zone the Rmf and Rxo can be used.

$$\frac{\textit{Mudfiltrate}}{\textit{Shortnormal}} \dots \textit{or} \dots \frac{R_{XO}}{R_{MF}} \dots \textit{or} \dots \frac{C_{MF}}{C_{XO}} = \varphi^{-m}$$

Or:

$$\log \varphi = \frac{\log(C_{MF} / C_{XO})}{-m} \dots \textit{valued} \dots \log \frac{(4545 / 323)}{-2}$$

Then..... $\varphi = 0.27$

6) Are the values found in 5a) and 5b) minimum or maximum values?

Answer:

C_{fw} > C_{mf}, 35714 > 4545 mmho/m

Invasion of mudfiltrate ((C_{mf}) causes:

-Induction conductivity will be too low.

-Correction could result in 2000 mmho/m.

Then:

$$\log \varphi = \frac{\log(C_{MF} / C_o)}{-m} \dots \text{valued} \dots \log \frac{(35714 / 2000)}{-2}$$

Then..... $\varphi = 0.237$

Similar Conductivity of the “short normal” correction would result in a lower porosity than 0.27