

Ca 3220 Final Exam: Spring 2013 Solution

1. a) This is unsteady cond. in a flat plate w/ insulated side.

Using FT, p. 130, we want $\frac{T_s - T_c}{T_s - T_0} = \frac{20 - 19.5}{20 - 15} = \frac{.5}{5} = 0.1$ *

$\rightarrow Fo \approx 0.26$, $Fo = \frac{\alpha t}{D^2} = \left(\frac{0.68}{1000 \cdot 4190}\right) \frac{t}{(0.005)^2} = (1.62 \cdot 10^{-7}) \frac{t}{10^{-6}} = 0.25 \cdot 10^{-2} t$
 * 2×0.001 to account for insulated surface

6.40 s

b) We need overall U (heat-transfer coef.) for water layer only 1 layer, no convection, $U = \left(\frac{0.001}{0.68}\right)^{-1} = 680 \text{ W/m}^2\text{K}$

Mass balance on Al layer: $AU(T_s - T) = A \Delta x \rho c_p \frac{dT}{dt}$
 (note sign is right: $T_s = 20^\circ\text{C} > T \rightarrow dT/dt > 0$).

$(680)(T_s - T) = (0.005)(2700)(938) \frac{dT}{dt} = -1.266 \cdot 10^4 \frac{dT}{dt}$
 $\frac{d(T_s - T)}{(T_s - T)} = -\frac{680}{1.266 \cdot 10^4} dt = -\frac{U}{\Delta x \rho c_p} dt$ Note balance is on Al plate. P, Cp refer to Aluminum

$\ln(T_s - T) = -0.0537 t + C$
 at $t=0$, $(T_s - T) = 5^\circ\text{C}$; thus $C = \ln 5$

$\ln\left(\frac{T_s - T}{5}\right) = -0.0537 t = \ln\left(\frac{0.5}{5}\right) = -2.302$
 $t = 42.8 \text{ s}$

c) This is same as pt a, but with different α and D .

We want $\frac{T_s - T_c}{T_s - T_0} = 0.1$ $Fo = 0.26 = \frac{\alpha t}{D^2}$ **

$\alpha = \frac{230}{2700 \cdot 938} = 9.08 \cdot 10^{-5} \rightarrow 0.26 = \frac{(9.08 \cdot 10^{-5}) t}{(0.010)^2} = 0.908 t$

0.28 s.

d) Slowest step is conduction across the water layer; $t \approx 43 \text{ s}$.
 Actual time is longer, because all these steps are in series.
 (But probably not much longer, because magnitudes are so different).

* Using BSL Fig 12.1-1 for part (a), we want $\frac{\alpha t}{b^2} \approx 1.0$, $b = 0.001 \text{ m}$
 ** " " " " " " $b = 0.005$

Same final answers.

This problem was motivated by an actual lab apparatus. The conclusion is that if we wait about a minute, it's OK.

2. Initial change sets dimensionless T's: $T_i = 0^\circ\text{C}$, $T_o = 100$.

At 30 min., it has been 30 min. since first change.

$\kappa = 9.08 \cdot 10^{-5}$ as in problem 1 (c).

$$\text{After 30 min, } \frac{\kappa t}{D^2} = \frac{(9.08 \cdot 10^{-5}) 30 \cdot 60}{(1.5)^2} = 0.0726 = F_0$$

$$\text{From FT p. 130, } \frac{T_i - T_c}{T_i - T_o} \approx 0.1; \quad \frac{T_c - T_o}{T_i - T_o} = 0.9$$

(From BSL Fig 12.1-3, $\frac{\kappa t}{R^2} = 0.79$; $\frac{T_c - T_o}{T_i - T_o}$ at center ≈ 0.87)

It has been 20 min since 2nd change.

$$\frac{\kappa t}{D^2} = \frac{(9.08 \cdot 10^{-5}) 20 \cdot 60}{(1.5)^2} = 0.0484$$

$$\text{From FT p. 130, } \frac{T_i - T_c}{T_i - T_o} \approx 0.30; \quad \frac{T_c - T_o}{T_i - T_o} = 0.70$$

(From BSL Fig 12.1-3, $(\kappa t/R^2) = 0.193$; $\frac{T_c - T_o}{T_i - T_o} \approx 0.69$)

$$\frac{T_c - T_o}{T_i - T_o} = (0.9) - (0.7) = 0.20 \quad T_c = 80^\circ\text{C}$$

3. Need a macro balance on sphere, since sphere is always at uniform T.

$$b) -A\sigma e(T^4 - T_o^4) + V S = V \rho c_p \frac{dT}{dt} \quad A = 4\pi R^2; \quad V = \frac{4}{3}\pi R^3$$

heat out (note sign) gen. accum

$$-4\pi R^2 \sigma e (T^4 - T_o^4) + \left(\frac{4}{3}\pi R^3\right) S = \left(\frac{4}{3}\pi R^3\right) \rho c_p \frac{dT}{dt}, \quad \text{Divide by } 4\pi R^2$$

$$-\sigma e (T^4 - T_o^4) + \frac{R}{3} S = \frac{R}{3} \rho c_p \frac{dT}{dt}$$

c) The final s.s. is when generation = heat lost, and $\frac{dT}{dt} = 0$.

$$A\sigma e(T^4 - T_o^4) = V S \rightarrow 4\pi R^2 \sigma e (T^4 - T_o^4) = \frac{4}{3}\pi R^3 S$$

$$(T^4 - T_o^4) = \frac{R S}{3 \sigma e}; \quad T = \left[\frac{R S}{3 \sigma e} + T_o^4 \right]^{1/4}$$

4. We don't know V or D_h , so this is trial + error.

$$D_h = 4 \frac{V}{(1+1+1)} = \frac{4}{3} V$$

$$Re = D_h V \rho / \mu = \left(\frac{4}{3} V\right) V \cdot 1000 / 0.001 = 1.333 \cdot 10^6 V$$

$$\dot{V} = \left(\frac{D_h}{L} \frac{2 \Delta P}{\rho} \frac{1}{4f} \right)^{1/2}$$

$$\frac{\Delta P}{L} = \rho g \cos(87^\circ) = 1000 (7.8) (0.0573) = 572.9$$

$$V = \left(\frac{(4/3)}{1000} \frac{2(572.9)}{\rho} \frac{1}{4f} \right)^{1/2} = (1.368/4f)^{1/2}; \quad E/D = \frac{0.05}{(4/3)} = 0.0375$$

$$\text{Guess } V = 1 \text{ m/s, } Re = 1.33 \cdot 10^6 \quad 4f \approx 0.06; \quad V = 4.77 \text{ m/s}$$

$$4.77$$

$$6.36 \cdot 10^6$$

$$0.06$$

$$4.77 \text{ m/s}$$

$$Q = VA = 4.77 \text{ m}^3/\text{s}$$

5. This problem is analogous to heat transfer in tube flow.

What is Re? $Re = \frac{Dv\rho}{\mu} = \frac{(1 \cdot 10^{-4})(5 \cdot 10^{-5})1000}{0.001} = 0.005$. Nearly laminar.

Are we relatively close to equl.?
 No.

$$No. \frac{(Q - C_A^p)}{Q - C_A^f} = 0.5 > 0.25$$

i. Can use analog to Eq. 3.124

$$Nu = 0.332 Re^{1/2} Pr^{0.33} \rightarrow Sh = 0.332 Re^{1/2} Sc^{0.53}$$

$$Sc = \frac{\mu}{R D} = \frac{0.001}{1000 \cdot 10^{-9}} = 1000; Sh = 0.332(0.005)^{1/2}(1000)^{0.53} = 0.235$$

Using "Eq. III" in notes,

$$"Nu_{eq} = Sh = \ln\left(\frac{Q - C_A^p}{Q - C_A^f}\right) Re Sc \frac{D}{4L}$$

$$0.235 = \ln(2)(0.005)(1000) \frac{10^{-4}}{4L}$$

$$L = 3.69 \cdot 10^{-4} \text{ m} \quad (370 \mu\text{m})$$

6. In highly turbulent flow, f becomes independent of Re.

a)

$$f = \text{const} \rightarrow v = \left(\frac{D}{L} \frac{\Delta P}{\rho} \frac{1}{4f}\right)^{1/2} = \text{constant} \left(\frac{\Delta P}{L}\right)^{1/2}$$

$$\text{or } \frac{\Delta P}{L} = \text{const.} \times v^2. \text{ Doubling } Q \rightarrow \frac{\Delta P}{L} \text{ rises } 4x.$$

b) For a power-law fluid, Q is proportional to $\left(\frac{\Delta P}{L}\right)^{1/n}$.

or $\left(\frac{\Delta P}{L}\right)$ is proportional to Q^n . If Q doubles and $\left(\frac{\Delta P}{L}\right)$ rises by 4x, then $n=2$. He thinks he's got a shear-thickening fluid.

7. a) Assume flow is up:

$$p_{\text{inlet}} = 6.105$$

$$p_{\text{outlet}} = 2.105$$

pipe rises, so must subtract effect of gravity.

$$\frac{\Delta P}{L} = \frac{(6.105 - 2.105) - 1000(9.8)100}{1000} = -\frac{5.80 \cdot 10^5}{1000} = -580 \text{ Pa/m} \quad (\text{if flow is up})$$

b) assumption was wrong. Flow is down, or from right to left.